

For near-Earth gravity, of course,

$$\vec{F}_{\text{ext.}} = \sum m_i \vec{g} = M \vec{g}$$

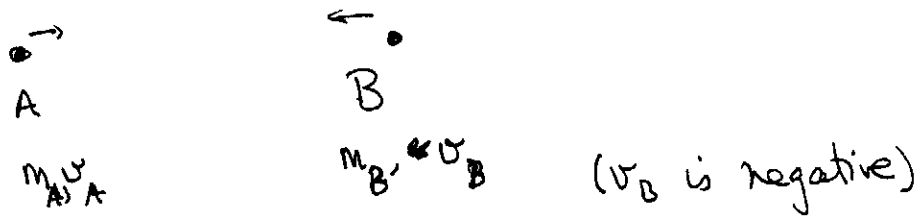
so  $\ddot{\vec{r}}_{\text{CM}} = \vec{g}$  !

(exp'ts.)

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example: collisions

$$\vec{F}_{\text{ext.}} = 0, \quad \underline{\underline{\vec{v}_{\text{CM}} = \text{const.}}}$$



$$\text{CM. : } \frac{m_A \vec{x}_A + m_B \vec{x}_B}{m_A + m_B}$$

its velocity:

$$\frac{m_A \vec{v}_A + m_B \vec{v}_B}{m_A + m_B}$$

after collision:  $\vec{v}'_A, \vec{v}'_B$

$$\text{but } \frac{m_A \vec{v}'_A + m_B \vec{v}'_B}{m_A + m_B} = \frac{m_A \vec{v}_A + m_B \vec{v}_B}{m_A + m_B}$$

$$m_A \vec{v}_A + m_B \vec{v}_B = \text{conserved. (momenta, total momentum.)}$$

# Applications

A) method of measuring mass!

$$m_A v_A' + m_B v_B' = m_A v_A + m_B v_B$$

$$m_A/m_B = \frac{v_B - v_B'}{v_A' - v_A}$$

3) inelastic collisions: All you need...

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# 25] Reformulation of Newton's Momentum

(Actually, <sup>this is</sup> Newton's original formulation!)

$$\vec{F} = \frac{d m \vec{v}}{dt} = \frac{d \vec{p}}{dt} \quad \vec{p} = m \vec{v}$$

Correction to CM:

$$\begin{aligned} \vec{P} &= M \vec{v}_{CM} \\ &= \sum m_i \vec{v}_i \\ &= \sum m_i \vec{x}_i \end{aligned}$$

Advantages: more advanced theories (relativity)

$$\frac{d \frac{m_0 \vec{v}}{\sqrt{1-v^2/c^2}}}{dt}$$

angular motion

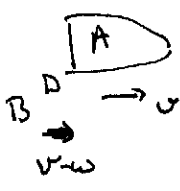
variable mass problems

$$\vec{F}_{ext.} = \frac{d(\vec{P}_A + \vec{P}_B)}{dt} = \frac{d \vec{P}_A}{dt} + \frac{d \vec{P}_B}{dt}$$

can divide it up "ad lib"

"dd" exhaust can be ignored!

example: rocket



$$\begin{aligned} 0 &= \frac{d \vec{P}_{rocket}}{dt} + \frac{d \vec{P}_{exhaust}}{dt} \\ &= \frac{d}{dt} (M-kt) \vec{v} + k(\vec{v}-\vec{w}) \\ &= (M-kt) \frac{d \vec{v}}{dt} - k \vec{w} \end{aligned}$$

specialize to 1 component

$$dv = \frac{k\omega}{M - kt} dt$$

$$v - v_0 = \omega \ln \frac{M}{M - kt} = \omega \ln \frac{1}{1 - \frac{kt}{M}}$$

$\omega = 0$  ✓

### 26) Generalized Conservation

$$\vec{F}_{ext.} = \frac{d}{dt} \vec{P}_{tot.}$$

$$\vec{P}_{tot.} = \sum m_i \vec{v}_i$$

$\Rightarrow \vec{P}_{tot.} = \text{const. if } \vec{F}_{ext.} = 0$

also more generally,  $(\vec{P}_{tot.})_i = \text{const. if } (\vec{F}_{ext.})_i = 0$

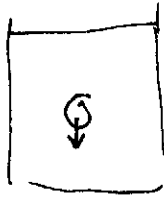
ex: near-earth gravity  $\vec{g} = -g \hat{z}$

$(\vec{P}_{tot.})_x, (\vec{P}_{tot.})_y = \text{conserved.}$

Smooth wall ~~(no friction)~~ [by the way: wall motion...]

$\vec{F}$   
 $x=z=0$   $(\vec{P}_{tot.})_x, (\vec{P}_{tot.})_z = \text{const. (neglecting gravity)}$   
 $(\vec{P}_{tot.})_x = \text{const. (even with gravity)}$

Example: honey pot

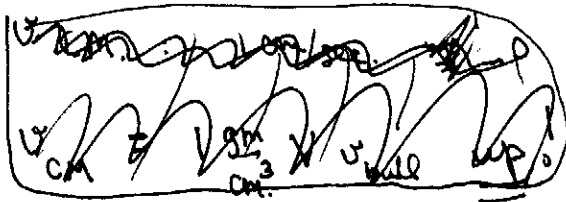


$$P_{\text{honey}} = \rho g h V_{\text{honey}}?$$

$$P_{\text{ball}} = \rho g h V_{\text{ball}}, V$$

$$V = \text{mass} \downarrow \text{ball}$$

momentum of honey?



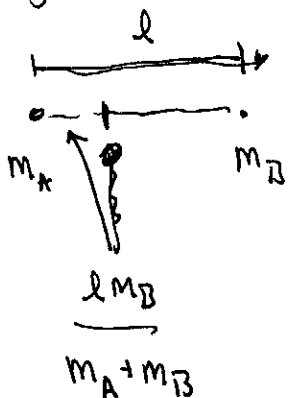
add extra bit  $(\rho_h - \rho_b)V, \vec{v}$

then no change in flow, no change in CM position!

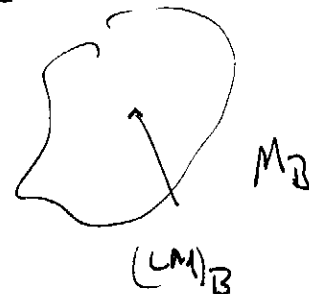
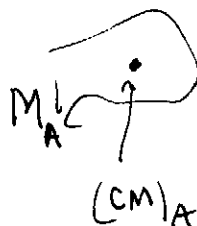
$$\text{so } \rho_b V \vec{v} + (\rho_h - \rho_b) V \vec{v} + \vec{P}_{\text{honey}} = M \dot{x}_{\text{CM}} = 0$$

$$\text{and } \vec{P}_{\text{honey}} = -\rho_h V \vec{v} !$$

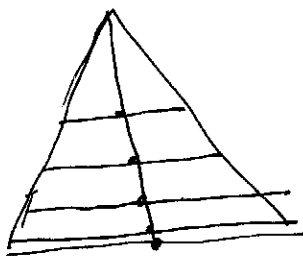
# 27] Finding the CM



← Also for system



uniform triangles  
- intersection of  
bisectors!



$$\vec{x}_{CM}^A = \frac{\sum_{i \in A} m_i \vec{x}_i}{\sum_{i \in A} m_i} \quad \vec{x}_{CM}^B = \frac{\sum_{i \in B} m_i \vec{x}_i}{\sum_{i \in B} m_i}$$

$$\vec{x}_{CM}^{A+B} = \frac{\sum_{i \in A+B} m_i \vec{x}_i}{\sum_{i \in A+B} m_i}$$

need not be a point in the system



$$m_A \vec{x}_{CM}^A + m_B \vec{x}_{CM}^B = (m_A + m_B) \vec{x}_{CM}^{A+B}$$

$$\vec{x}_{CM}^{A+B} = \frac{m_A \vec{x}_{CM}^A + m_B \vec{x}_{CM}^B}{m_A + m_B}$$

sectors (chords, ~~edges~~ slices, wedges)

chord



$$M = 2R\theta$$

$$M h = \int_{-\theta/2}^{\theta/2} R \cos \phi R d\phi = 2R^2 \sin \theta \Rightarrow h = \frac{R \sin \theta}{\theta}$$

$\theta = 0, \pi, 2\pi$

slice



$$dM = \sigma 2\theta r dr \quad M = \sigma R^2 \theta$$

$$\frac{dM}{hdM} = \frac{r \sin \theta}{\theta} \sigma 2\theta r dr = 2\sigma \sin \theta r^2 dr$$

$$\int hdM = \frac{2}{3} \sigma R^3 \sin \theta$$

$$H = \frac{\frac{2}{3} \sigma R^3 \sin \theta}{\sigma R^2 \theta} = \frac{2}{3} R \frac{\sin \theta}{\theta}$$

wedge

$$dM = \rho 2\pi r^2 \sin \theta (1 - \cos \theta) dr$$



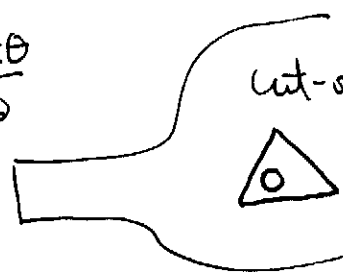
$$M = \frac{2\pi \rho}{3} (1 - \cos \theta) R^3$$

$$hdM = \rho 2\pi r^2 (1 - \cos \theta) dr \times \frac{r \sin \theta}{\theta}$$

$$M \theta H = \frac{\rho \pi}{2} \frac{(1 - \cos \theta) \sin \theta}{\theta}$$

$$\theta H = \frac{3}{4} R \frac{\sin \theta}{\theta}$$

state but don't do



cut-outs

$$M_r \vec{x}_r^{CM} + m_c \vec{x}_c^{CM} = M_{whole} \vec{x}_{whole}^{CM}$$
$$M_r \vec{x}_{CM} = M_{whole} \vec{x}_{whole}^{CM} - m_c \vec{x}_c^{CM}$$

Physical determination:

hang it anywhere, plumb line passes through CM  
(proof later)

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## 28) Center of Mass Frame

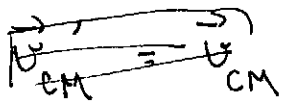
i) Invariance of the equations : "Galilean relativity"

$$\vec{r}'_i = \vec{r}_i - \vec{v}t \quad \vec{F}' = \vec{F}$$

$$t' = t$$

$$\frac{d^2 \vec{r}_i}{dt^2} = \vec{F}_{i, \text{ext.}} + \vec{F}_{ij} [\vec{r}_i - \vec{r}_j]$$

↓ same thing      ↓ same thing      ↓ same thing !



$$\text{ii) } \vec{r}'_{\text{CM}} = \vec{r}_{\text{CM}} - \vec{v}t$$

$$\left( = \frac{\sum m_i \vec{r}'_i}{\sum m_i} = \frac{\sum (m_i \vec{r}_i - m_i \vec{v}t)}{\sum m_i} = \vec{r}_{\text{CM}} - \vec{v}t \right)$$

$$\vec{v}'_{\text{CM}} = \vec{v}_{\text{CM}} - \vec{v}$$

choose  $\vec{v} = \vec{v}_{\text{CM}}$

Things are often simpler to analyze in CM frame.  
You can always transform back at the end.



~~24) Elastic~~

29) Elastic Collisions (Slightly Unconventional)

Invariance of the equations

$$\vec{r}'_i(t) = \vec{r}_i(-t) \quad \vec{F}'_i = \vec{F}$$

$$\text{[2]} t' = -t$$

$$\Rightarrow \frac{d\vec{r}'_i(t)}{dt'} = - \frac{d\vec{r}_i(-t)}{dt}$$

$$\frac{d^2\vec{r}'_i(t)}{dt'^2} = + \frac{d^2\vec{r}_i(-t)}{dt^2}$$

But: friction? inelastic collisions?

Internal Motion

For stiff bodies, we can neglect this. Then in CM, things "bounce back" (possibly rotated) w same velocities.

(If smaller velocities, time-reverse has bigger velocities: too good to be true!)

Start with

$$m_1, \vec{v}_1$$

lab frame, before

$$m_2, \vec{v}_2$$

← N.B: 1d vectors (sign mts!)

move to CM frame; use velocity  $\vec{v}$  such that

$$m_1(\vec{v}_1 - \vec{v}) + m_2(\vec{v}_2 - \vec{v}) = 0$$

$$\vec{v} = \frac{m_1 \vec{v}_1 + m_2 \vec{v}_2}{m_1 + m_2}$$

$$\text{so } \vec{v}_1 - \vec{v} = \frac{m_2(\vec{v}_1 - \vec{v}_2)}{m_1 + m_2} \quad \text{etc.}$$

CM frame, before

$$m_1, \frac{m_2(\vec{v}_1 - \vec{v}_2)}{m_1 + m_2}$$

$$m_2, \frac{m_1(\vec{v}_2 - \vec{v}_1)}{m_1 + m_2}$$



CM frame, after

$$m_1, \frac{m_2(\vec{v}_2 - \vec{v}_1)}{m_1 + m_2}$$

$$m_2, \frac{m_1(\vec{v}_1 - \vec{v}_2)}{m_1 + m_2}$$

now go back to lab frame: add  $\vec{v}$

lab frame, after

$$m_1, \left( \frac{m_2(\vec{v}_2 - \vec{v}_1)}{m_1 + m_2} + m_1 \vec{v}_1 + m_2 \vec{v}_2 \right)$$

$$m_2, \frac{2m_1 \vec{v}_1 + (m_2 - m_1) \vec{v}_2}{m_1 + m_2}$$

$$\frac{(m_1 - m_2) \vec{v}_1 + 2m_2 \vec{v}_2}{m_1 + m_2}$$

if  $m_2/m_1 \rightarrow \infty$

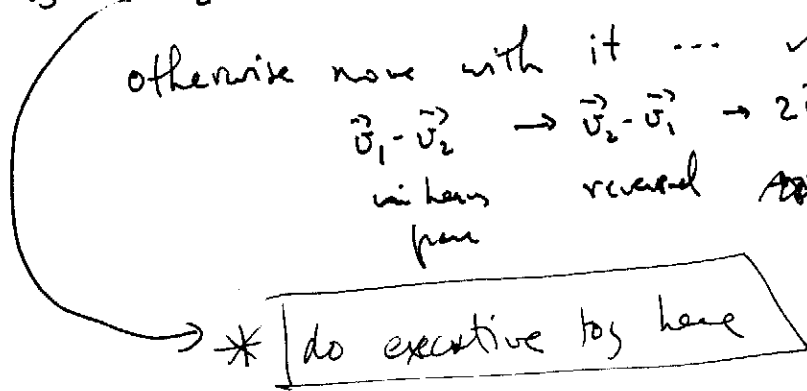
$$m_1, -\vec{v}_1 + 2\vec{v}_2 \quad | \quad m_2, \vec{v}_2$$

~~argue~~  $\vec{v}_2 = 0 \checkmark$

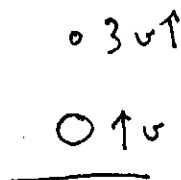
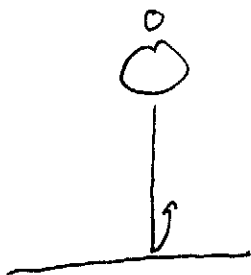
otherwise move with it ...  $\checkmark$

$$\vec{v}_1 - \vec{v}_2 \rightarrow \vec{v}_2 - \vec{v}_1 \rightarrow 2\vec{v}_2 - \vec{v}_1$$

in hand      reversed      ~~Arg~~ back to lab



Example: Superbounce!



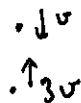
$$S_v = \frac{v^2}{2g}$$

$$S_{3v} = 9 S_v !!$$

3 balls



90v



7v

49 times!

4 balls

$$(15^2) = 225 \text{ times!}$$

$$n \text{ balls } (2^n - 1)^2 \text{ times!}$$

equal matters?

$$\begin{array}{c} \downarrow 0 \\ \downarrow \vec{v} \\ \uparrow 0 \end{array} \rightarrow \begin{array}{c} \uparrow 0 \\ \downarrow \vec{v} \end{array} \rightarrow \begin{array}{c} 0 \uparrow \vec{v} \\ 0 \uparrow \vec{v} \end{array}$$

"executive toy"

$$\begin{array}{c} 0 \\ m, \vec{v} \end{array} \quad \begin{array}{c} 0 \\ m, 0 \end{array}$$



$$\begin{array}{c} 0 \\ m, 0 \end{array} \quad \begin{array}{c} 0 \\ m, \vec{v} \end{array}$$

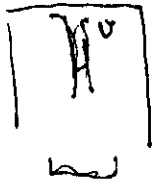
prove to  $\Phi$ ,  
7.36

### 30] Impulse

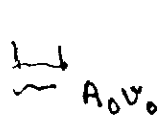
$$\Delta \vec{P} = \int \vec{F} dt$$

This can be useful when the LHS is "obvious".

ex:



$$\underbrace{\rho A v}_{\Delta m} v = \rho A v^2$$



$$v = \sqrt{v_0^2 - 2gh}$$

$$\begin{aligned} [v &= v_0 - gt ; t = \frac{v_0 - v}{g} \\ h &= v_0 t - \frac{1}{2} g t^2 \end{aligned}$$

$$\begin{aligned} &\frac{1}{g} [v_0(v_0 - v) - \frac{1}{2}(v_0 - v)^2] \\ &= \frac{1}{2g} (v_0^2 - v^2) \end{aligned}$$

ex: trampoline



$$\Delta P = 0 \quad \int_0^T (\vec{F}_{\text{tramp, ma.}} dt + m\vec{g} dt)$$

$$\int_0^T \vec{F}_{\text{tramp, ma.}} dt = -m\vec{g} T$$

$$\frac{1}{T} \int_0^T \vec{F}_{\text{tramp, ma.}} dt = +m\vec{g}$$

ex: origin of pressure



same idea

### 31) General Comments on Energy

- i) forces, <sup>+ dynamics</sup> as function of position, as opposed to time.
- ii) like momentum, a much more general principle beyond classical mechanics
- iii) can be 'hidden' or dissipated; or stored.

This contrasts with momentum

iv) ~~internal~~ forces do not cancel in general

### 32) Work-Energy Theorem: Particles

$$m \ddot{\vec{r}} = \vec{F}(\vec{r})$$

dot-product with  $d\vec{r} = \dot{\vec{r}} dt$

$$m \ddot{\vec{r}} \cdot \dot{\vec{r}} dt = \vec{F} \cdot d\vec{r}$$

$$\frac{m}{2} \frac{d}{dt} (\dot{\vec{r}} \cdot \dot{\vec{r}}) dt = \frac{d}{dt} \left( \frac{m}{2} v^2 \right)$$

$$\int_A^B : \frac{m}{2} (v_B^2 - v_A^2) = \int_A^B \vec{F} \cdot d\vec{r}$$

$$\Delta \text{ kinetic energy} = \text{work}$$

### 33) Analysis of Cases

The work-energy theorem is <sup>especially</sup> ~~most~~ useful when we can evaluate the right-hand side without having to solve for the motion! where this applies:

↑ These are several important cases  
This is not true in general, of course.

o) If several force-types act, total work = sum of partial works (4)

i) force-fields in 1 dimension

$$\int_A^B \vec{F}(x) \cdot d\vec{x} = \int_A^B F(x) dx$$

Let  $\Delta V$   $V(x) \equiv -\int_{x_0}^x F(x) dx$ , so  $F(x) = -\frac{dV}{dx}$

Then  $work_A^B = -(V(B) - V(A)) = -\Delta V$   
 $= -\Delta$  (potential energy)

$\Rightarrow \Delta$  (kinetic energy + potential energy)

= work by other forces

Note:  $V$  contains an arbitrary constant

examples:

Spring  
 particle attached to

$$F(x) = -k(x - x_0)$$

$$V(x) = \frac{1}{2} k(x - x_0)^2$$

Typically, we choose it to vanish at a convenient "natural" place  
 $\leftarrow V=0$  at equil. pt.

nearby-earth gravity, vertical motion

$$F(z) = -mg$$

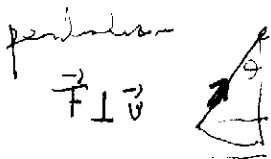
$$V(z) = mgz \leftarrow \text{(to vanish at } z=0)$$



Newtonian gravity, vertical motion

$$F(r) = -\frac{GMm}{r^2}$$

$$V(r) = -\frac{GMm}{r} \leftarrow \text{(to vanish at } r = \infty)$$



$$V(\theta) = mgl(1 - \cos\theta)$$

$$K = \frac{1}{2} m l^2 \dot{\theta}^2$$

$K + V = \text{const.}$ ; take  $\frac{d}{dt} \Rightarrow$  eq<sup>n</sup> of motion



iii) conservative force-fields in 3d

If  $\int_A^B \vec{F}(\vec{r}) \cdot d\vec{r}$  depend only on the endpoints, not on the path, we say the force-field is conservative.

spring (0 size, not origin)

$$\vec{F}(\vec{r}) = -k\vec{r}$$

$$\vec{F}(\vec{r}) \cdot d\vec{r} = -k\vec{r} \cdot d\vec{r} = -\frac{1}{2} k dr^2$$

so  $V(\vec{r}) = \frac{1}{2} kr^2$

near-earth gravity

$$\vec{F}(\vec{r}) = -mg\hat{z}$$

$$\vec{F}(\vec{r}) \cdot d\vec{r} = -mg dz$$

$$V(\vec{r}) = mgz \implies \text{any "1d" force}$$

Newtonian gravity (fixed source)

$$\vec{F}(\vec{r}) = -\frac{GMm}{r^2} \hat{r}$$

use  $\hat{r}, \hat{\theta}, \hat{\phi}$  basis (also note an argument in plane)

$$\vec{F}(\vec{r}) \cdot d\vec{r} = -GMm d(-\frac{1}{r}) = GMm d(\frac{1}{r})$$

$$V(\vec{r}) = -\frac{GMm}{r}$$

example: escape velocity